

Kinetic Studies of Air Column Acoustics

R. Dean Ayers and Mark T. McLaughlin

Department of Physics and Astronomy, California State University Long Beach, Long Beach, CA 90840-3901, USA

The linear behavior of an air column can now be illustrated very easily using a personal computer. Concepts that may have been somewhat abstract become more concrete with kinetic images on the computer screen. One basic example is a representation of standing waves with imperfect nodes in terms of several dependent variables, each of which displays a "lurching" or "galloping" behavior. Because of the emphasis that they receive in introductory courses, undamped traveling waves and ideal standing waves can play too prominent a role in a student's understanding of realistic waves, which are subject to damping in propagation and on reflection. A detailed examination of the intermediate "lurching" waves may help to relegate those idealized special cases to their proper roles as limiting behaviors. The treatment of the example presented here is analytic rather than numerical, with the computer just providing kinetic images of the solutions. The use of scrollbar controls for physical parameters of the wave images encourages informal experimentation. Allowing students to write their own program lines for the calculation of dependent variables may help them to make the transition from using real sinusoids to working with complex exponentials.

"LURCHING" WAVE BEHAVIOR

Two undamped sinusoidal plane waves of the same wavelength λ propagate in opposite directions in a uniform pipe. All acoustic pressures are normalized to the amplitude of the stronger wave, which travels to the right (+x direction). The amplitude of the weaker wave is R , the pressure reflection coefficient at the origin, and here R is limited to positive values. Thus at time $t = 0$ both pressure waves have crests at $x = 0$. At each point in the region $x < 0$, where the waves overlap, the total acoustic pressure varies sinusoidally in time. The amplitude of that temporal variation is

$$A_p(x) = [1 + R^2 + 2R\cos(2kx)]^{0.5}, \quad (1)$$

where the propagation number $k = 2\pi/\lambda$. Imperfect nodes and antinodes are visible in the amplitude envelope, which is the pair of broken curves $\pm A_p(x)$ in Fig. 1. (The value $R = 0.5$ results from dividing the area of the pipe's cross section by three for $x > 0$.)

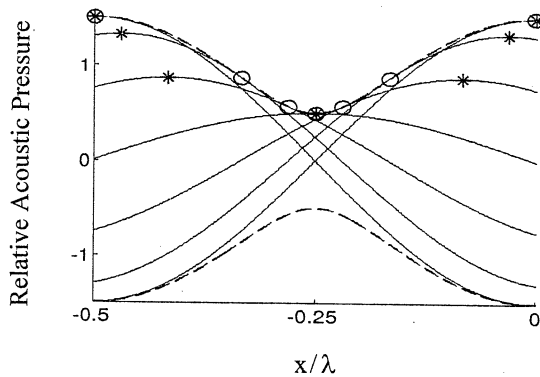


FIGURE 1. Amplitude envelope (broken) and lurching wave plots (solid) for $R = 0.5$: * = crest; o = contact point.

Each frame in a moving picture of the total disturbance is a sinusoidal function of x . A few of these are shown at an interval of $\Delta t = T/12$ from $-T/2$ to 0, with $T =$ the period. The height of a crest in the total wave (*) must vary as it shifts in order to squeeze through each node. The curve traced by a crest is

$$p_{\text{crest}}(x) = (1 - R^2)/[1 + R^2 - 2R\cos(2kx)]^{0.5}. \quad (2)$$

The velocity of the total wave varies, whether one focuses on a crest or on a point of contact with the upper envelope curve (temporal maximum, o). For either type of feature the average velocity over a half period is $v = \lambda/T$ to the right. Within that interval the variation can be considerable, as shown in Fig. 2. Crests travel rapidly through nodal regions and slowly near antinodes, while temporal maxima show the opposite behavior. The two normalized velocities have the same time dependence except for a shift by $T/4$:

$$v_{x, \text{feature}}/v = (1 - R^2)/[1 + R^2 \pm 2R\cos(2\omega t)], \quad (3)$$

with + for a crest, - for a contact point, and $\omega = 2\pi/T$.

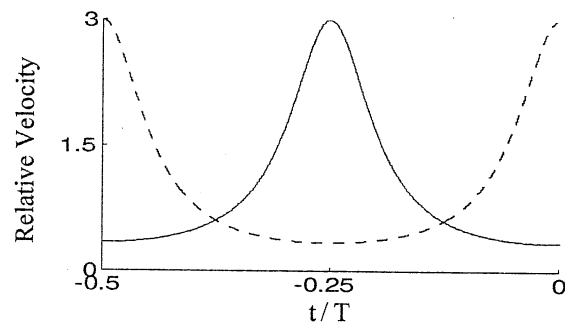


FIGURE 2. Normalized feature velocities: solid = crest; broken = contact (temporal maximum).

The behavior of the normalized particle velocity is similar to that of the acoustic pressure. In this example its reflection coefficient at $x=0$ is just $-R$, so we can adapt the results obtained for pressure. The amplitude envelope for $x < 0$ gets shifted by $\lambda/4$, placing a node at $x=0$, and the signs for the two velocities in Eq. (3) are exchanged.

The antinodes and nodes of the two amplitude envelopes are the only locations where acoustic pressure and particle velocity are in phase with each other, as in a single traveling wave. At those points the lurching wave can be coupled *without reflection* to an incident wave in an upstream pipe of appropriate diameter. For the odd integer multiples of $\lambda/4$ between a node and an antinode, the diameter of the lurching wave segment must be the geometric mean of the diameters on either side of it to avoid reflection. For the integer multiples of $\lambda/2$ between two antinodes or two nodes, the diameters upstream and downstream from the lurching wave segment must be equal.

ENERGY AND INTENSITY

The potential and kinetic energy densities also show lurching behavior. Their normalized values

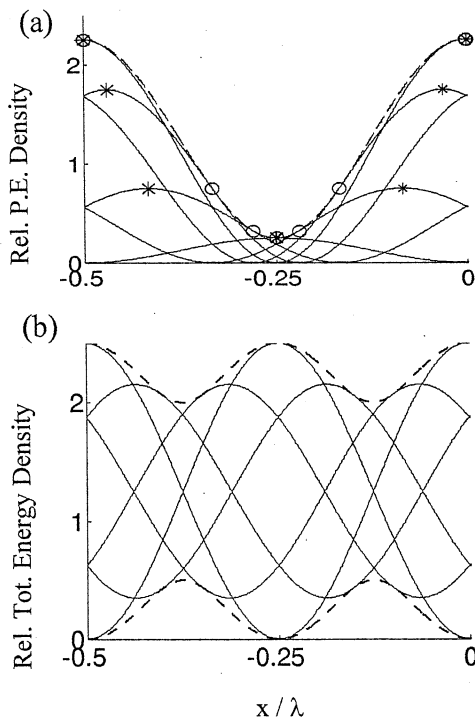


FIGURE 3. Lurching behaviors of energy densities and their envelopes: (a) potential energy density, (b) total energy density; $R = 0.5$ and $\Delta t = T/12$ for $-T/2 < t < 0$.

are just the squares of the normalized acoustic pressure and particle velocity, respectively. The potential energy density and its envelope are shown in Fig. 3(a). The kinetic energy density has the same envelope shape, but shifted by $\lambda/4$. The total energy density and its envelope are shown in Fig. 3(b). Finally, Fig. 4 shows the envelope and instantaneous plots for the acoustic intensity, $p v_{x,\text{particle}}$, the power flux per unit area. The horizontal lines at 0 and 1 are the upper limits for the two envelope curves, independent of the value of R .

IMPLEMENTATION AND USES

The software was developed in MATLAB,[®] version 6. Scrollbar controls on the screen for R and other parameters make this a hands-on tool. Students can check their solutions to analytic problems by writing program lines for calculating the dependent variables. Those who are just learning to use complex exponentials can verify that they give the same results as real sinusoids. This software is also useful for studying waves in higher dimensions, or those with damping in propagation. Input impedance, pressure reflection coefficient, and effective length, all treated as functions of axial position as well as frequency, can also be examined in non-uniform air columns.

ACKNOWLEDGMENTS

This work has been supported by the Paul S. Veneklasen Research Foundation and the CSULB Scholarly and Creative Activities Committee. We are grateful to Nader Inan for his assistance.

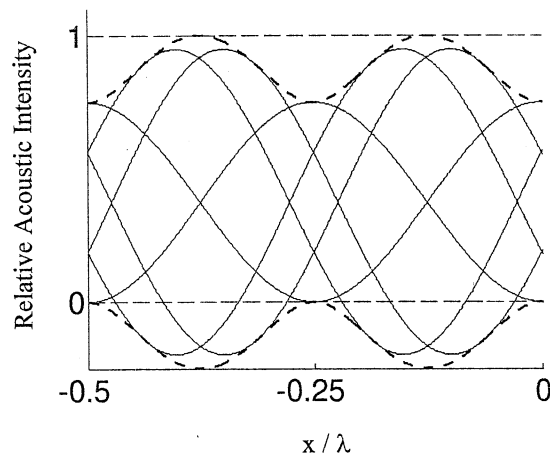


FIGURE 4. Acoustic intensity and envelope.